

Mechanical Behavior of Recycled Concrete Aggregates (RCA) for Improved Sustainability of Reinforced Concrete Building Structures











Environmental Considerations of Recycled Concrete Aggregates (RCA) for Improved Sustainability of Reinforced Concrete Building Structures

Mark Davis

Andres de la Rosa University of Texas at Tyler

Dr. Michael McGinnis

Dr. Yahya C. Kurama University of Notre Dame

Dr. Brad Weldon New Mexico State University









College of Engineering



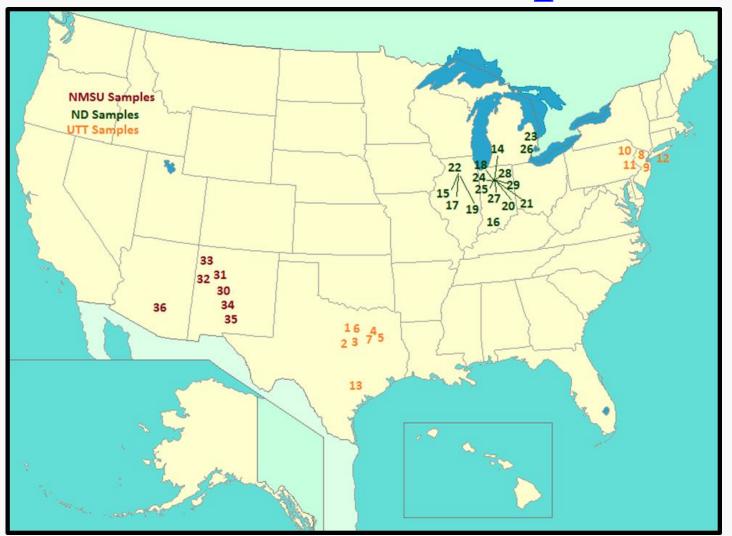
Outline

- RCA Sample Collection
- Sample & Target Gradations
- Natural Aggregate (NA) & Recycled Concrete Aggregate (RCA) Properties
- Mix Designs
- 28-Day Compressive Strength Results
- Relationship between Theoretical Values and Measured Values





Collected Samples









BCL - 3" (TX)



BCB - Base (TX)







CCF - 1.5" Minus (PA)



CCN - 1.5" to 0.375" Minus (PA)





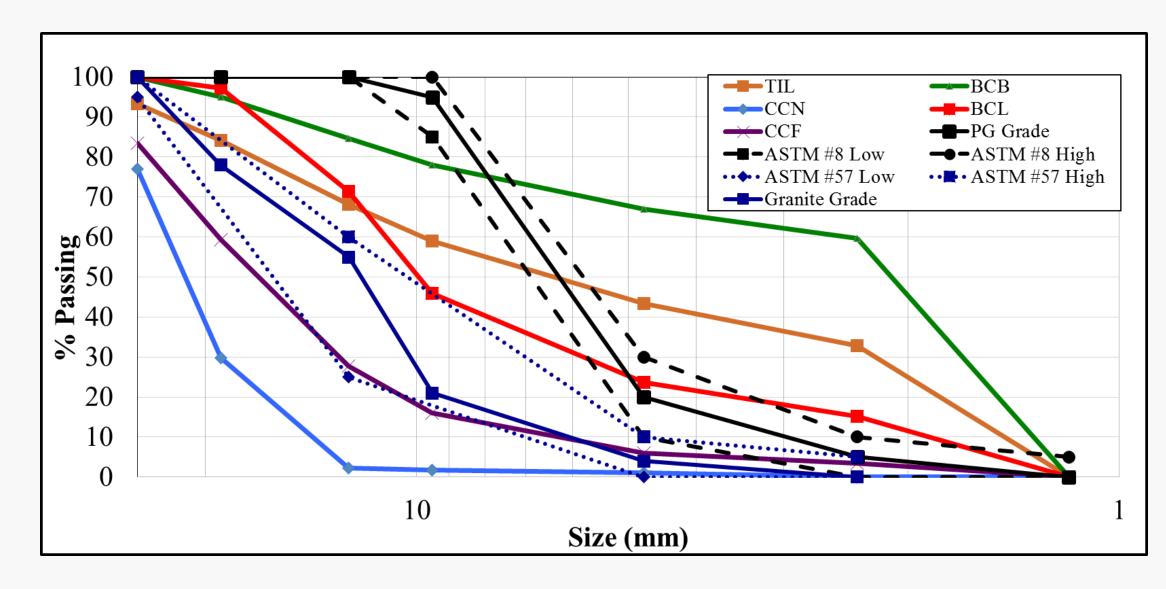


TIL - 1.5" Minus (NJ)





Gradations







Natural Aggregate (NA) and Recycled Concrete Aggregate (RCA) Properties

| State of Origin | Sample | Type | Absorption | Bulk SG | Bulk SSD | Apparent SG | DRCA (%) |
|--------------------|--------|------|------------|---------|----------|-------------|----------|
| NJ | TIL | RCA | 5.41 | 2.31 | 2.43 | 2.64 | 4.63 |
| PA | CCF | RCA | 5.01 | 2.33 | 2.45 | 2.64 | 5.95 |
| PA | CCN | RCA | 5.02 | 2.33 | 2.44 | 2.63 | 10.33 |
| TX | ВСВ | RCA | 5.95 | 2.28 | 2.42 | 2.64 | 2.29 |
| TX | BCL | RCA | 5.52 | 2.29 | 2.42 | 2.62 | 2.96 |
| TX | PG | NA | 1.83 | 2.55 | 2.60 | 2.68 | N/A |
| TX | Sand | NA | 1.00 | 2.62 | 2.65 | 2.69 | N/A |





NA and RCA Properties

| State of Origin | Sample | Type | Absorption | Bulk SG | Bulk SSD | Apparent SG | DRCA (%) |
|-----------------|--------|------|------------|---------|----------|-------------|----------|
| NJ | TIL | RCA | 5.41 | 2.31 | 2.43 | 2.64 | 4.63 |
| PA | CCF | RCA | 5.01 | 2.33 | 2.45 | 2.64 | 5.95 |
| PA | CCN | RCA | 5.02 | 2.33 | 2.44 | 2.63 | 10.33 |
| TX | ВСВ | RCA | 5.95 | 2.28 | 2.42 | 2.64 | 2.29 |
| TX | BCL | RCA | 5.52 | 2.29 | 2.42 | 2.62 | 2.96 |
| TX | PG | NA | 1.83 | 2.55 | 2.60 | 2.68 | N/A |
| TX | Sand | NA | 1.00 | 2.62 | 2.65 | 2.69 | N/A |





NA and RCA Properties

| State of Origin | Sample | Type | Absorption | Bulk SG | Bulk SSD | Apparent SG | DRCA (%) |
|-----------------|--------|------|------------|---------|----------|-------------|----------|
| NJ | TIL | RCA | 5.41 | 2.31 | 2.43 | 2.64 | 4.63 |
| PA | CCF | RCA | 5.01 | 2.33 | 2.45 | 2.64 | 5.95 |
| PA | CCN | RCA | 5.02 | 2.33 | 2.44 | 2.63 | 10.33 |
| TX | ВСВ | RCA | 5.95 | 2.28 | 2.42 | 2.64 | 2.29 |
| TX | BCL | RCA | 5.52 | 2.29 | 2.42 | 2.62 | 2.96 |
| TX | PG | NA | 1.83 | 2.55 | 2.60 | 2.68 | N/A |
| TX | Sand | NA | 1.00 | 2.62 | 2.65 | 2.69 | N/A |





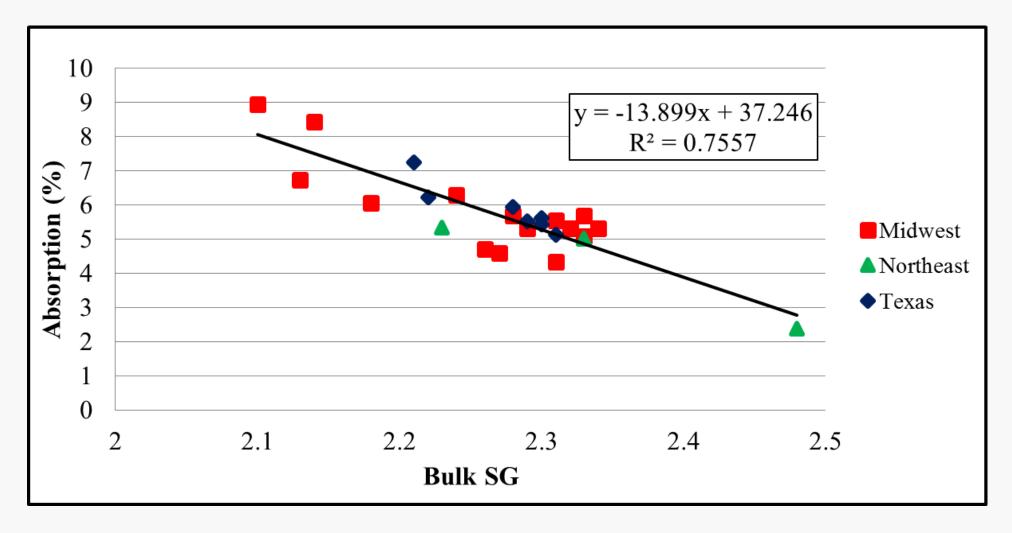
NA and RCA Properties

| State of Origin | Sample | Туре | Absorption | Bulk SG | Bulk SSD | Apparent SC | DRCA (%) |
|-----------------|--------|------|------------|---------|----------|-------------|----------|
| NJ | TIL | RCA | 5.41 | 2.31 | 2.43 | 2.64 | 4.63 |
| PA | CCF | RCA | 5.01 | 2.33 | 2.45 | 2.64 | 5.95 |
| PA | CCN | RCA | 5.02 | 2.33 | 2.44 | 2.63 | 10.33 |
| TX | ВСВ | RCA | 5.95 | 2.28 | 2.42 | 2.64 | 2.29 |
| TX | BCL | RCA | 5.52 | 2.29 | 2.42 | 2.62 | 2.96 |
| TX | PG | NA | 1.83 | 2.55 | 2.60 | 2.68 | N/A |
| TX | Sand | NA | 1.00 | 2.62 | 2.65 | 2.69 | N/A |





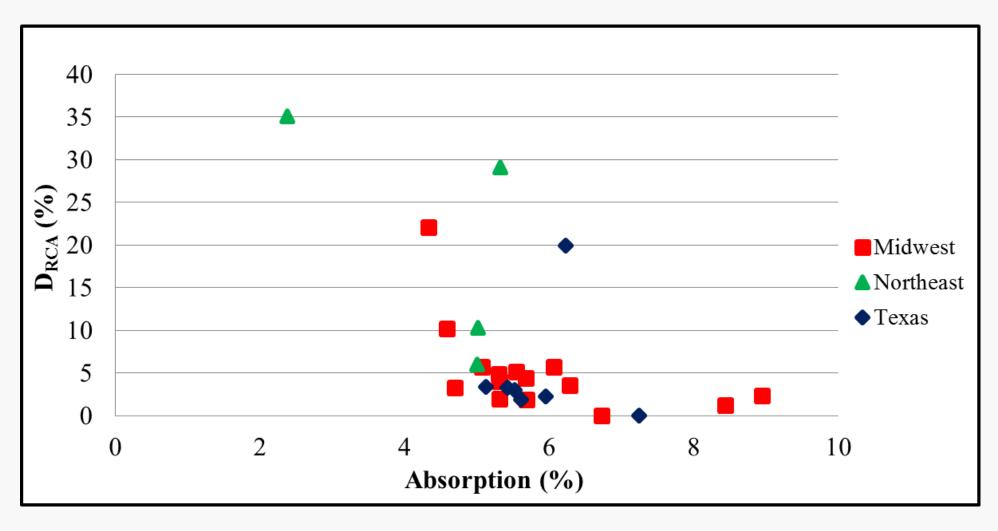
Absorption vs. Specific Gravity







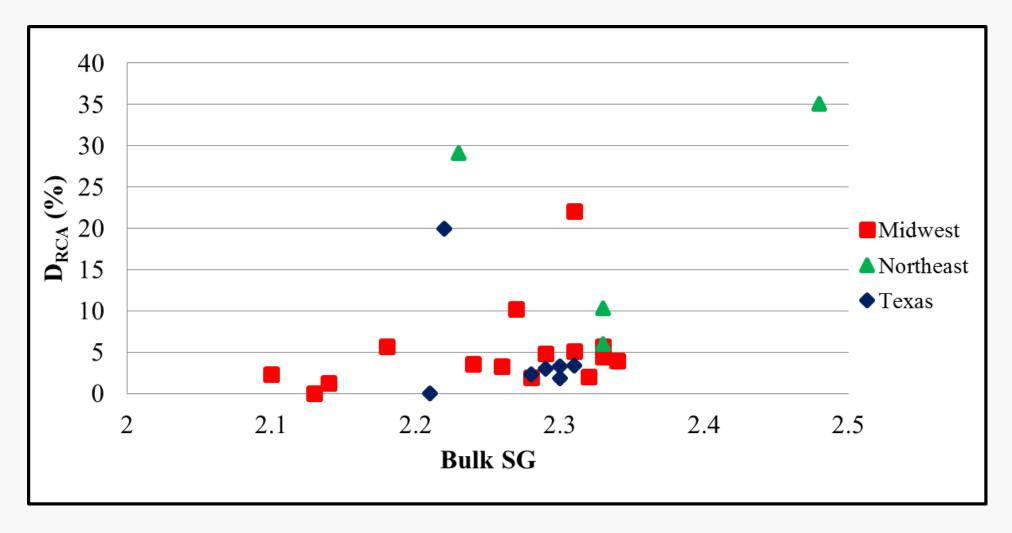
Deleterious Material (DRCA) vs Absorption







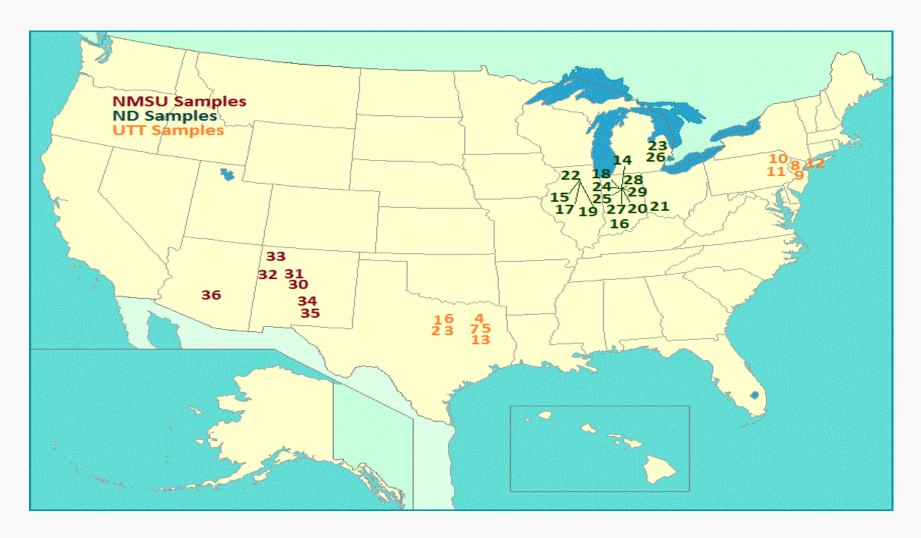
DRCA vs Bulk Specific Gravity







Collected Samples







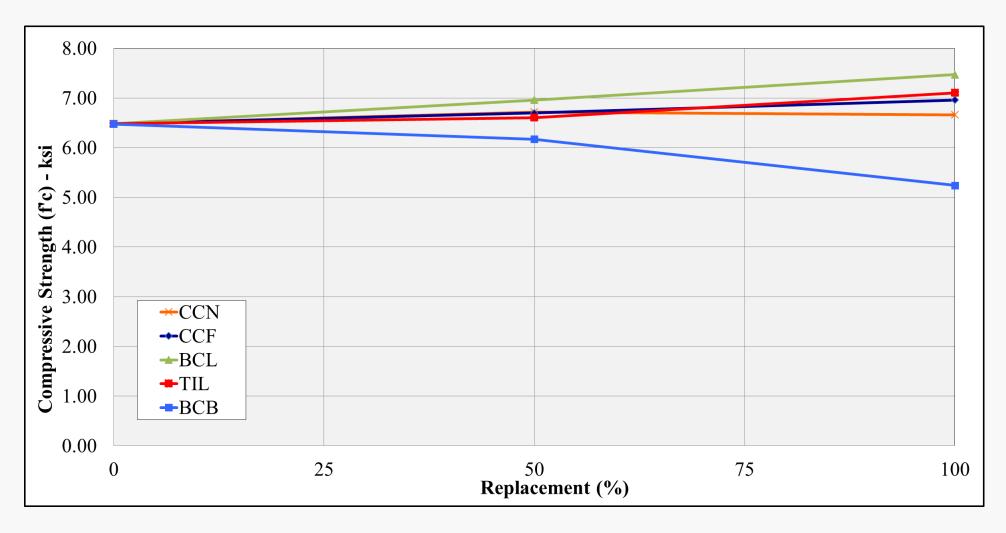
Mix Designs

| | PG Graded M1 Mixes | | | | | | |
|--------|--------------------|--------------|--------------|----------------|----------------|-------------------|-----------------------|
| Sample | Replacement (%) | PS 1466 (mL) | Cement (lbs) | CA Added (lbs) | FA Added (lbs) | Water Added (lbs) | Weight in Mixer (lbs) |
| PG | 0 | 7.79 | 4.40 | 11.80 | 9.96 | 0.553 | 26.7 |
| ВСВ | 50 | 7.89 | 4.45 | 12.30 | 9.94 | 0.000 | 26.7 |
| ВСВ | 100 | 7.99 | 4.51 | 12.02 | 10.11 | 0.098 | 26.7 |
| BCL | 50 | 7.89 | 4.44 | 11.90 | 10.10 | 0.260 | 26.7 |
| BCL | 100 | 7.99 | 4.51 | 11.85 | 10.25 | 0.093 | 26.7 |
| TIL | 50 | 7.89 | 4.45 | 11.80 | 10.15 | 0.30 | 26.7 |
| TIL | 100 | 7.99 | 4.50 | 11.90 | 10.25 | 0.049 | 26.7 |
| CCN | 50 | 7.89 | 4.45 | 11.95 | 9.98 | 0.297 | 26.7 |
| CCIV | 100 | 7.99 | 4.50 | 12.07 | 10.04 | 0.106 | 26.7 |
| CCF | 50 | 7.89 | 4.44 | 11.86 | 10.05 | 0.357 | 26.7 |
| CCI | 100 | 7.99 | 4.49 | 11.85 | 10.20 | 0.159 | 26.7 |





28 Day Compressive Strength







Prediction Equation

$$fc,RCA/fc,NA = \beta_{f1} + \beta_{f2} \times + \beta_{f3} \times D + \beta_{f4} \times R$$

| | βf_1 | 1.0241 | | βf_1 | [1.0026, 1.0456] |
|---------------------------------------|-------------|---------|---|-------------|--------------------|
| Mean Value of Unnormalized Regression | βf_2 | -0.0241 | 95% Confidence Interval For Unnormalized | βf_2 | [-0.0300 ,-0.0182] |
| Coefficients | βf_3 | -0.0138 | Regression Coefficients | βf_3 | [-0.0172, -0.0104] |
| | βf_4 | 0.0769 | | βf_4 | [0.0299,0.1239] |

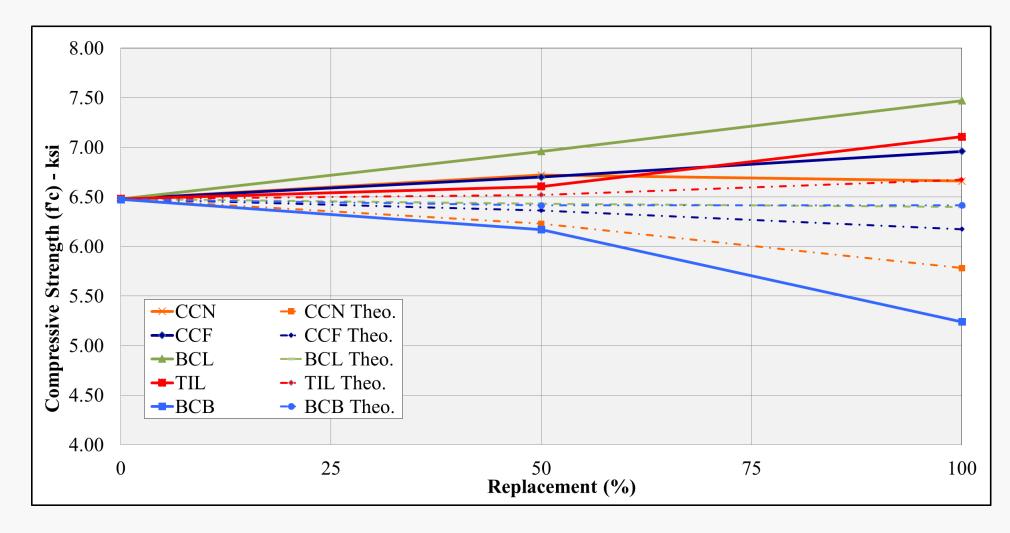
D = Combined deleterious material content of RCA

R = Replacement Percentage





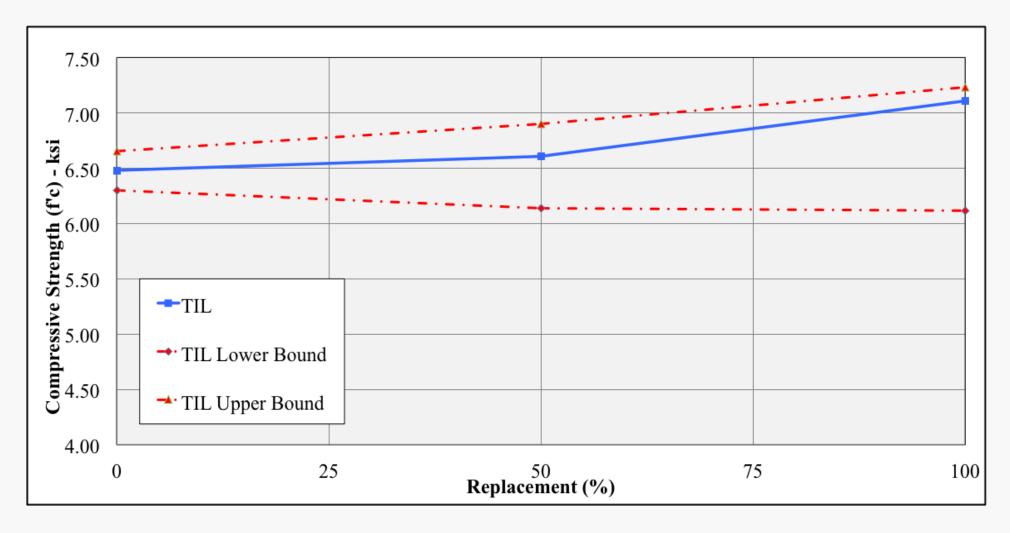
Measured vs. Theoretical







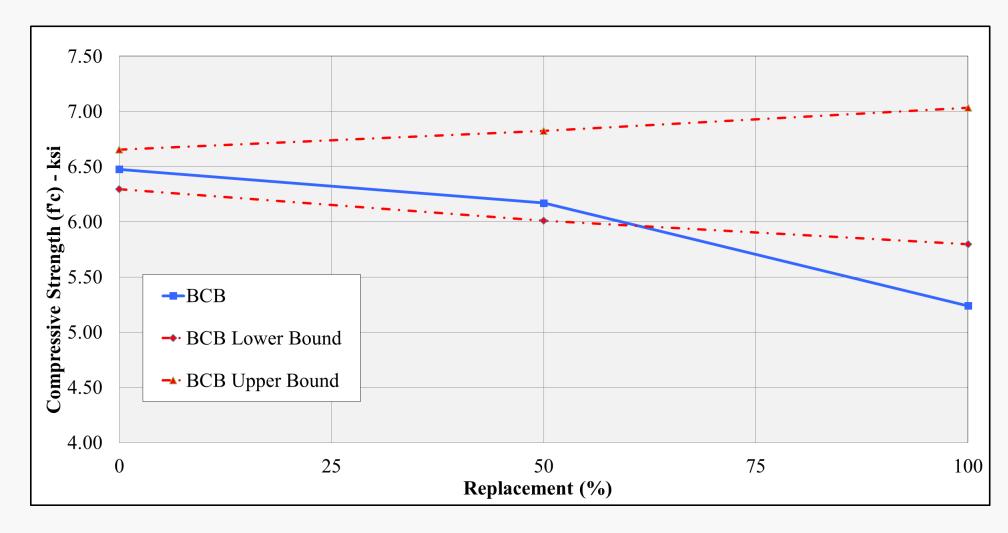
Confidence Intervals







Confidence Intervals







Measured Values vs. Theoretical Values

| Sample | Measured f'c at 50% R | Theoretical f'c at 50% R | Percent Difference (%) | Measured c' at 100% R | Theoritical f'c at 100% R | Percent Difference (%) |
|--------|-----------------------------|--------------------------|------------------------------|-----------------------------|---------------------------------|------------------------------|
| ВСВ | 6.17 | 6.41 | -3.89 | 5.24 | 6.42 | 20.19 |
| BCL | 6.96 | 6.43 | 7.87 | 7.47 | 6.40 | 15.45 |
| CCF | 6.70 | 6.36 | 5.16 | 6.96 | 6.17 | 11.95 |
| CCN | 6.72 | 6.23 | 7.57 | 6.66 | 5.78 | 14.11 |
| TIL | 6.61 | 6.52 | 1.29 | 7.11 | 6.67 | 6.29 |





Measured Values vs. Theoretical Values

| Sample | Measured f'c at 50% R | Theoretical f'c at 50% R | Percent Difference (%) | Measured f'c at 100% R | Theoritical f'c at 100% R | Percent Difference (%) |
|--------|-----------------------------|--------------------------|------------------------------|------------------------------|---------------------------------|------------------------------|
| ВСВ | 6.17 | 6.41 | -3.89 | 5.24 | 6.42 | -20.19 |
| BCL | 6.96 | 6.43 | 7.87 | 7.47 | 6.40 | 15.45 |
| CCF | 6.70 | 6.36 | 5.16 | 6.96 | 6.17 | 11.95 |
| CCN | 6.72 | 6.23 | 7.57 | 6.66 | 5.78 | 14.11 |
| TIL | 6.61 | 6.52 | 1.29 | 7.11 | 6.67 | 6.29 |





RCA's Effect on Strength

| Sample | Percent Difference from 0% to 50% | Percent Difference from 0% to 100% |
|--------|-----------------------------------|------------------------------------|
| ВСВ | -4.82 | -21.2 |
| BCL | 3.71 | 2.82 |
| CCF | 3.42 | 7.20 |
| CCN | 7.22 | 14.3 |
| TIL | 2.00 | 9.29 |





Conclusions

- Quality concrete can be made with RCA following the DVR method. The strengths of the mixes with 50% RCA replacement differed from their NA counterparts by approximately \pm 10%; for 100% RCA replacement the difference was \pm 20%.
- A model created to predict the strength of RCA concrete mixes based on the absorption and DRCA of a subset of all available data needs further development this is future work planned by the project team.





Conclusions

- The variability of RCA properties available for purchase was reasonably large for gradation (many sold as road base or for other applications other than concrete making) and for deleterious material (ranging from 1.87% to 35.1% over the data set studied).
- The specific gravity of the RCA samples was also variable, ranging from 2.1 to 2.5
- The absorption of the RCA data set ranged from approximately to 10%, and it was linearly related to the RCA specific gravity.



College of Engineering



Acknowledgments

- National Science Foundation (NSF), http://www.nsf.gov/
- Project #: 1436758



